

New Busbar Network Concepts Taking Advantage of Copper Collector Bars to Reduce Busbar Weight and Increase Cell Power Efficiency

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Abstract

At the 2015 ICSOBA conference a reversed compensation current (RCC) busbar network concept was presented. There is no return potline as the full return current passes under the cells back to the rectifiers. The concept preferably uses upstream and downstream anode risers to produce a symmetric upstream/downstream steady-state bath-metal interface deformation. This busbar arrangement gives a very stable cell operation but requires more busbar weight.

In order to reduce the busbar weight, the concept has been improved by the use of copper collector bars, which allows extracting 100 % of the cell current on the downstream side of the cell and then feeding 50 % of the current to the standard upstream risers and 50 % to busbars passing under the next cell to the downstream risers. The improved concept has alternated upstream and downstream risers. It decreases busbar voltage drop and increases cell power efficiency.

This concept can also be used for the external compensation current (ECC) busbar design, which does not require downstream anode risers and reduces the busbar weight and cell voltage further. This paper presents detailed results for B_x , B_z , metal pad flow, cell voltage and power efficiency, for improved RCC and ECC concepts.

Keywords: MHD cell stability; busbar design; mathematical modeling; power efficiency; copper collector bars.

1. Usage of Copper Collector Bars

In its 2011 ALUMINIUM article [1], the author presented a 500 kA cell design using massive collector bar inserts, covering 76 % of steel collector bar cross-section (see Figure 1). At the time, it was speculative whether such a collector bar design could actually be built, but it is no longer the case today after Storvik AS publication at the ISCOBA 2015 conference, presenting technology for casting copper inserts into steel [2]. Furthermore, at the TMS 2016 conference KAN-NAK advocated that copper collector bars do not even need to be protected by steel shell and rodDED to the block with cast iron [3]. The results presented in Figure 8 of [1] demonstrated that the usage of copper bars having similar sizes as standard steel collector bars completely eliminate horizontal current in the metal pad while Figure 6 of [1] (reproduced in Figure 1 below) presents model prediction of a 63 mV cathode drop operation for that 500 kA cell.

1.1. Extracting 100 % of the cell current on the downstream side

What the author did not realized in 2011 is that with the usage of copper collector bars, 100 % of the cell current can be extracted on the downstream side without generating excessive horizontal current in the metal pad or generating excessive cathode voltage drop. In order to test this idea, the 3D thermo-electric model previously used in [1] was adapted keeping exactly the same lining design and collector bar size.

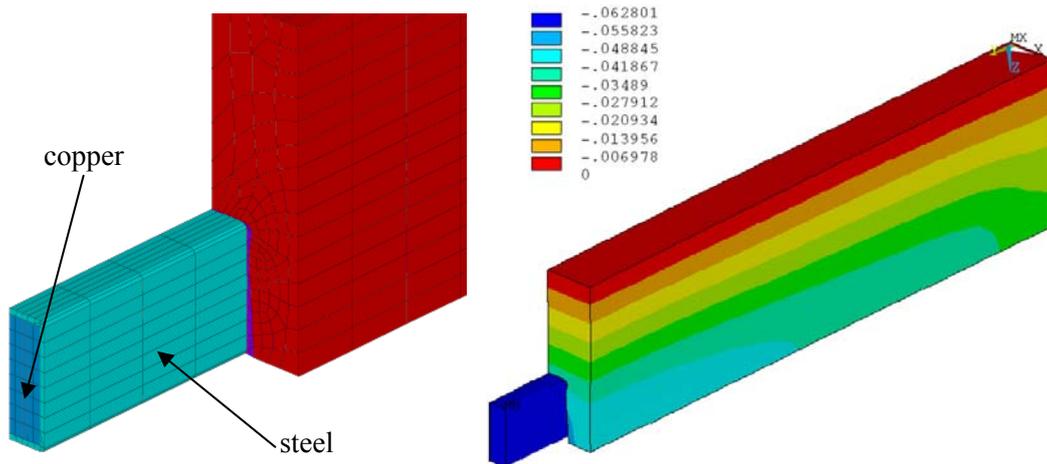


Figure 1. Thermo-electro-mechanical model with copper cross-section shown (left) and predicted cathode voltage drop (right from [1]).

The cell has now a single collector bar across the whole width of the pot. In the model, the carbon-cast iron contact resistances of $4 \mu\Omega\text{m}^2$ for the vertical interface and $8 \mu\Omega\text{m}^2$ for the horizontal interface were used. The resulting calculated current density when all the current is extracted from the downstream side is presented in Figure 2.

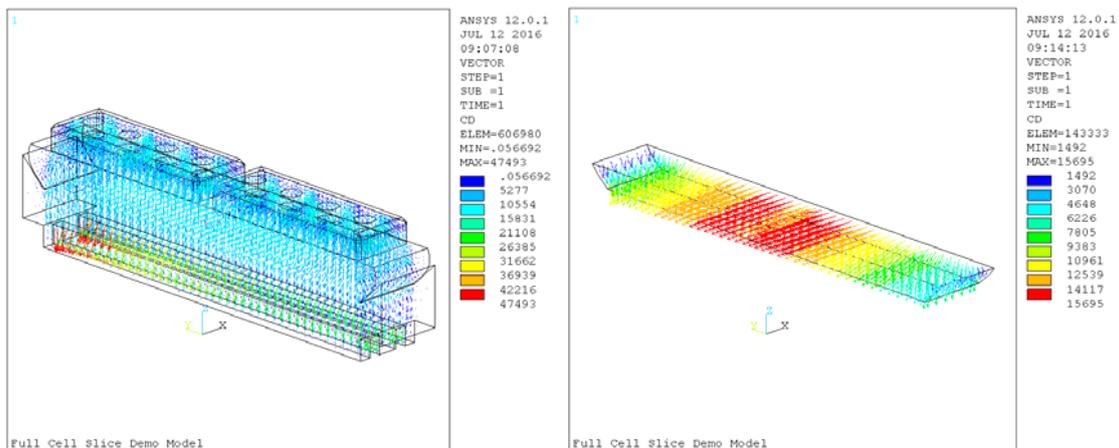


Figure 2. Thermo-electric model with current density in the whole domain (left) and in the metal pad only (right).

With that size of collector bars, the resulting horizontal current density in the metal pad has the same order of magnitude that the one obtained when using a standard steel collector bar designs. Figure 3 presents the predicted corresponding cathode voltage drop and temperature.

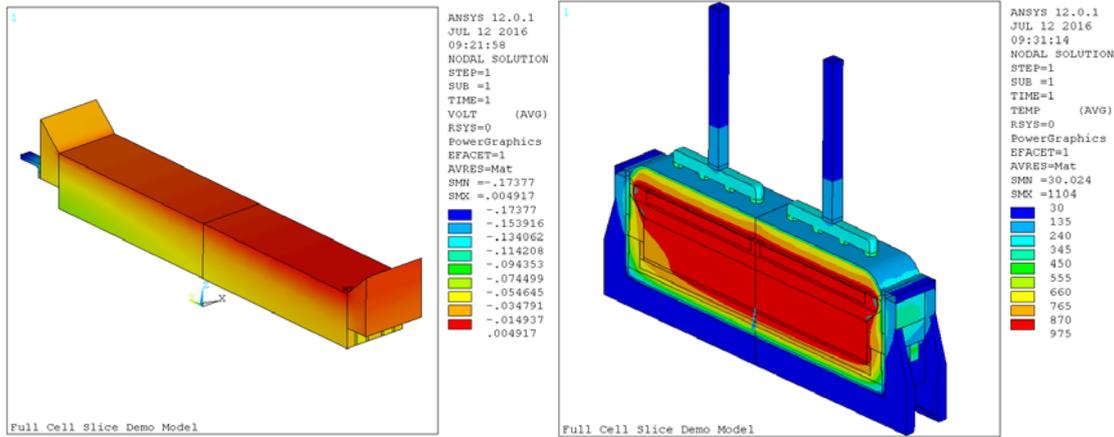


Figure 3. Thermo-electric model voltage drop (left) and temperature (right).

The cathode voltage drop is predicted to be 174 mV which is still a very low value despite the fact that now 100 % of the current is exiting the cell on the downstream side. Those results have been confirmed by MHD-Valdis model of the same configuration as part of the MHD cell stability study. Figure 4 shows the metal pad and cathode surface current density calculated by MHD-Valdis.

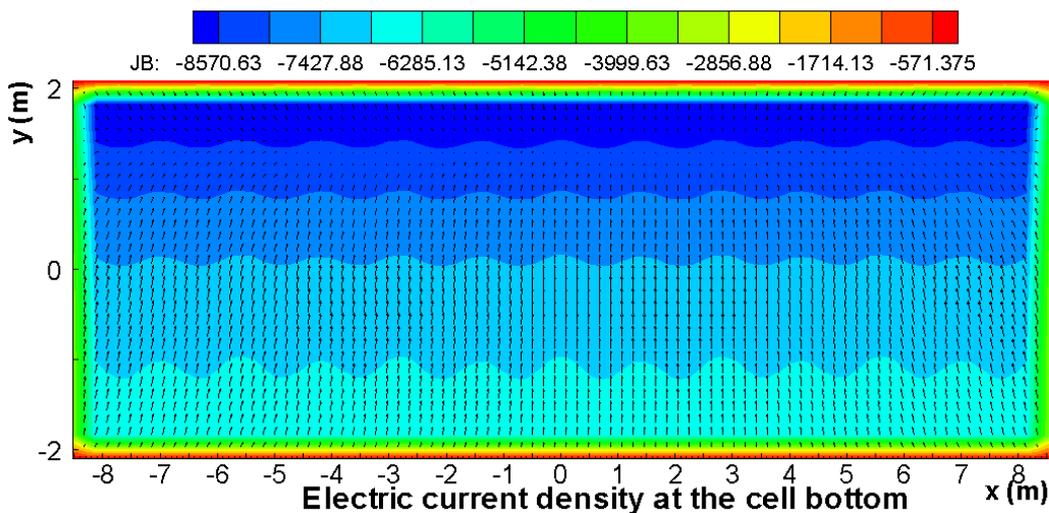


Figure 4. Current density calculated with MHD-Valdis. Contours: current density entering the cathode block. Arrows: Horizontal current density in the metal pad.

2. Busbar Network Designs Taking Advantage of 100 % Downstream Cell Current Extraction

2.1. Reversed compensation current (RCC) busbar network case

The initial RCC busbar network concept introduced at the last ICSOBA conference [4] is based on the usage of compensation busbar passing under the cells carrying 100 % of the cell line current but in the opposite direction. This introduces the option of building a smelter with a single potroom containing a single row of cells as the current can be returned to the rectifiers by the RCC busbar.

It was also discussed that that single innovation is producing very stable cell designs at any cell size and amperage as RCC compensation systematically generates a magnetic field in the metal

pad having a very small vertical components (B_z). Unfortunately using RCC without any other changes generated very asymmetric upstream/downstream steady-state bath-metal interface deformation (see Figure 11 of [4]).

In order to eliminate that potentially operational problem, a second innovation was introduced in [4], the usage of downstream risers. The introduction of such downstream risers corrects the shift in the longitudinal magnetic field component (B_x) generated by the RCC and produces a symmetric upstream/downstream steady-state bath-metal interface deformation.

Figure 5 shows one of the two possible busbar configurations using both RCC and downstream risers as proposed in [4]. In this busbar configuration, the current, coming from the downstream side of the cell, is going to the usual anode risers located on the upstream side of the next cell while the current coming from the upstream side of the cell is passing under that cell and the next cell to feed the new anode risers located on the downstream side of that next cell.

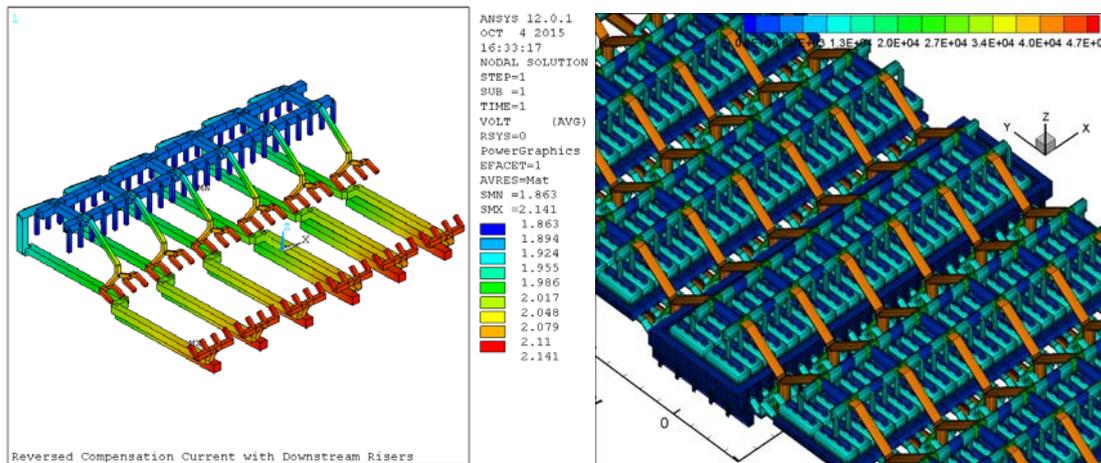


Figure 5. Original RCC busbar network concept with downstream risers [4].

While addressing all the MHD related design criteria for any cell size and amperage, the above configuration does require more busbar weight than existing busbar network designs. By taking advantage of the fact that with the usage of copper collector bars 100 % of the cell current can now exit on the downstream side of the cell, a new weight optimized RCC busbar network concept with downstream risers was developed. As in the first design, 50 % of the anode current is fed from the usual anode risers located on the upstream side and the other 50% is fed from the new anode risers located on the downstream side; but this time those risers are used in alternation, so they no longer face each other as it can be seen in Figure 6.

It can be noticed that the compensation busbars passing under the cell were not changed as that configuration produced the quite acceptable B_x and B_z components of the magnetic field presented in Figure 7. Other locations of the compensation busbar could be investigated.

That magnetic field combines with the current density field already presented in Figure 4 to produce the steady-state bath-metal interface deformation and metal pad steady state metal flow velocity field presented in Figure 8. The metal flow velocity field is quite unique to this new busbar configuration. It is characterized by multiple zones of higher speed below the center channel that would be obvious places to locate the point breaker feeders (PBF). That type of metal pad flow field should contribute to reduce the sludge accumulation under those PBF.

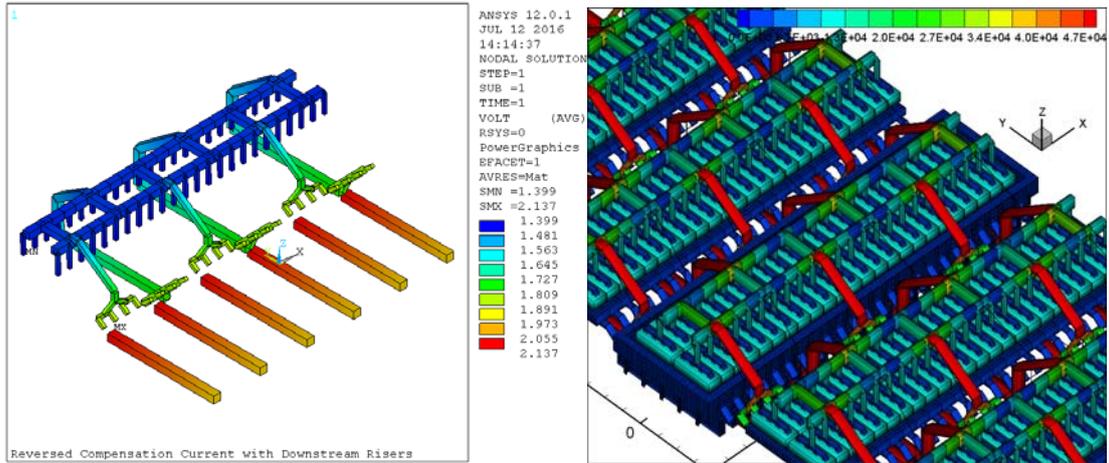


Figure 6. Optimized RCC busbar network concept with alternating risers.

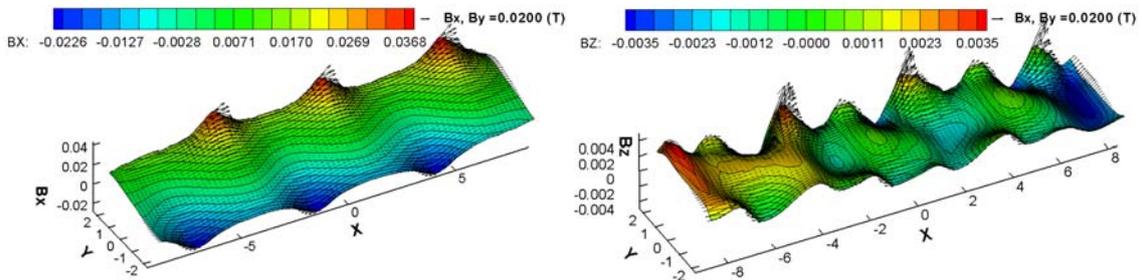


Figure 7. Corresponding B_x and B_z magnetic field components.

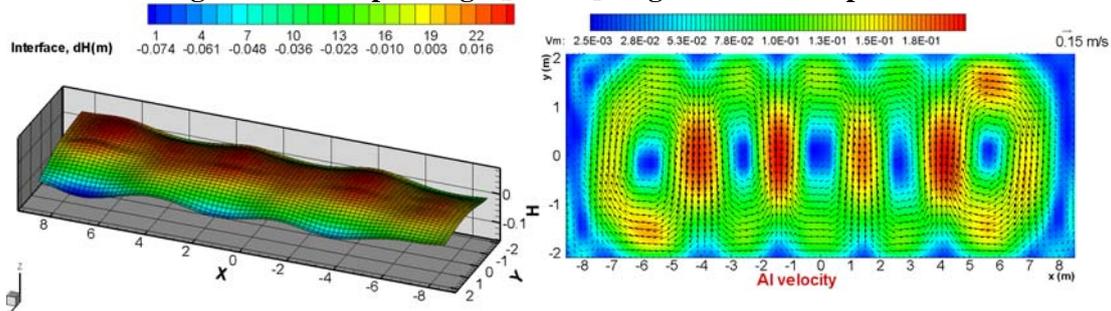


Figure 8. Corresponding steady-state bath-metal interface deformation and steady-state metal pad flow velocity field.

As for the cell energy consumption of that cell design with that new RCC busbar configuration and that new cathode design, the 500 kA cell presented in [1] that was the starting point of the current new cell design was predicted to operate at 12.1 kWh/kg (not reported in [1]) with its 87 mV cathode drop, its 265 mV anode drop and its 310 mV busbar drop (not reported in [1]). As previously presented, by extracting 100 % of the cell current on the downstream side without increasing the copper collector bar size, the cathode voltage drop is expected to increase to 174 mV. When using a similar busbar weight, the external busbar drop of the revised RCC is expected to be very similar to the ECC external busbar drop used in [1] so no adjustment is required for that external ohmic component. This means that that 500 kA cell with copper collector bars extracting 100 % of its current on the downstream side and using this revised alternating anode risers RCC busbar configuration is predicted to run at 12.4 kWh/kg while operating at the same 3.5 cm ACD reported in [1].

2.2. External compensation current (ECC) busbar network

While the idea of taking advantage of copper collector bars to extract 100% of the cell current on its downstream side came to the author as a way to reduce of busbar weight of its original RCC busbar configuration, it so happen that the same idea is easily applicable to existing ECC busbar configurations as well. Figure 9 presents such an ECC busbar configuration.

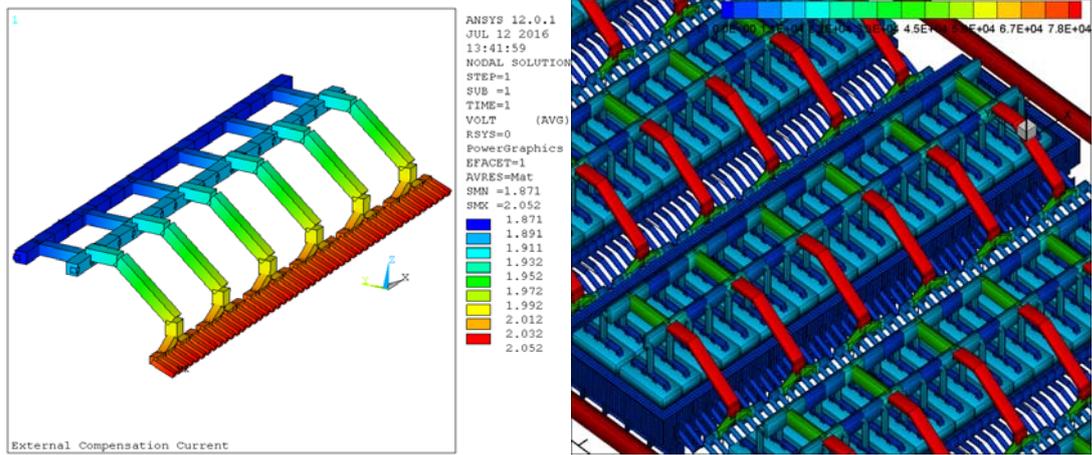


Figure 9. ECC busbar network concept with 100 % downstream side current exit.

The optimization of the busbar network is very simple as there is only one busbar component, so the resulting 180 mV of external busbar drop and busbar weight depend only on the choice of the busbar current density. The metal pad current density is not affected by the change of busbar network configuration from RCC to ECC as both are perfectly balanced and each are using components pulling the current from groups of four cathode blocks, so Figure 4 results stand for this ECC busbar configuration as well.

The resulting magnetic field depends on the current and location of the two compensation busbars and the location of the return line as it was the case for the results presented in Figure 2 of [1]. The magnetic field presented in Figure 10 was obtained without moving the location of the return line. The corresponding steady-state bath-metal interface deformation and metal pad steady-state metal flow velocity field are presented in Figure 11.

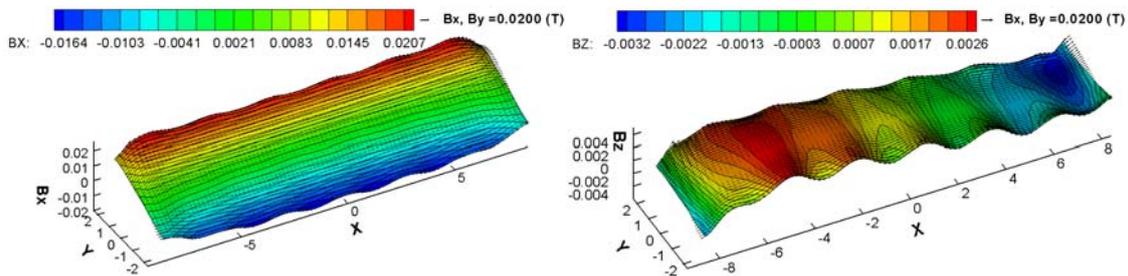


Figure 10. B_x and B_z magnetic field components for ECC.

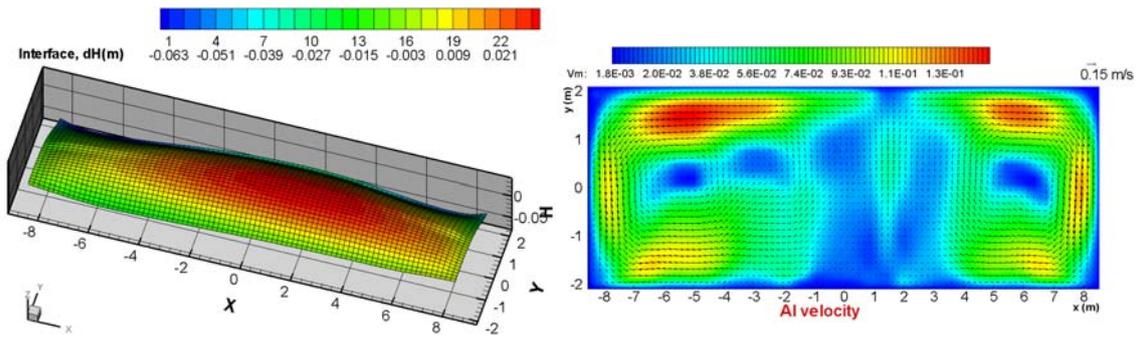


Figure 11. Steady-state bath-metal interface deformation and steady-state metal pad flow velocity field for ECC.

As compared to the previous RCC busbar network case, the change of the predicted cell energy consumption depends only on the change of the external busbar voltage drop as the cell design remained exactly the same. Assuming a reduction of 130 mV of the external busbar drop, the corresponding reduction of the cell energy consumption is 0.4 kWh/kg so that 500 kA cell with copper collector bars extracting 100 % of its current on the downstream side and using ECC busbar configuration is predicted to operate at 12 kWh/kg while operating at the same 3.5 cm ACD reported in [1].

A revised calculation was done using 3.2 cm of ACD instead of 3.5 cm as since 2011, indications are that ACD has been reduced further in low energy consumption cell prototypes. At an ACD of 3.2 cm, the predicted cell energy consumption is calculated to decrease to 11.7 kWh/kg Al.

3. Conclusions

The results presented demonstrated that the usage of copper collector bars with similar sizes as standard steel collector bars can be used to extract 100 % of the cell current on the cell downstream size without generating excessive horizontal current in the metal pad or generating excessive cathode voltage drop.

A 500 kA cell with copper collector bars extracting 100 % of its current on the downstream side and using a revised alternating anode risers RCC busbar configuration is predicted to be MHD stable and to run at 12.4 kWh/kg while operating at 3.5 cm ACD and 0.8 A/cm² of anode current density.

From [4] it can be extrapolated that a 740 kA or a 1500 kA cell with copper collector bars extracting 100 % of its current on the downstream side and using the same type of revised alternating anode risers RCC busbar configuration would work equally well at the same level of power efficiency.

A 500 kA cell with copper collector bars extracting 100 % of its current on the downstream side and using a revised ECC busbar configuration is predicted to be MHD stable and to run at 12 kWh/kg while operating at 3.5 cm ACD or 11.7 kWh/kg while operating at 3.2 cm ACD and 0.8 A/cm² of anode current density.

4. References

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